

# HIGH PERFORMANCE DUAL OPERATIONAL AMPLIFIER

- LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION

#### **DESCRIPTION**

The LS204 is a high performance dual operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high Gain-Bandwidth Product.

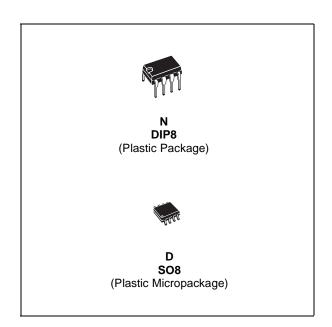
The circuit presents very stable electrical characteristics over the entire supply voltage range, and is particularly intended for professional and telecom applications (active filter, etc).

### **ORDER CODE**

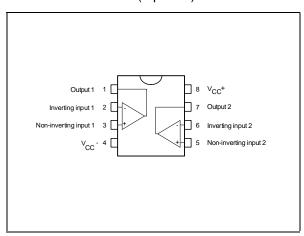
Part Number	Temperature Range	Package						
Fait Number	Temperature Nange	N	D					
LS204C	0°C, +70°C	•	•					
LS204I	-40°C, +105°C	•	•					
Example: LS2	Example: LS204CN							

N = Dual in Line Package (DIP)

**D** = Small Outline Package (SO) - also available in Tape & Reel (DT)

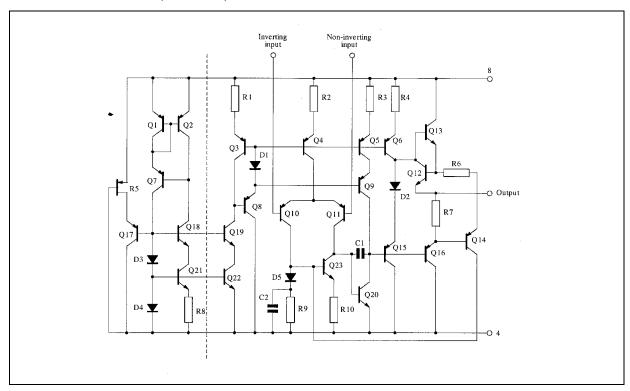


### PIN CONNECTIONS (top view)



November 2001 1/10

## **SCHEMATIC DIAGRAM** (1/2 LS204)



### **ABSOLUTE MAXIMUM RATINGS**

Symbol	Parameter	Value	Unit
V <sub>CC</sub>	Supply voltage	±18	V
V <sub>i</sub>	Input Voltage	±V <sub>CC</sub>	V
$V_{id}$	Differential Input Voltage	±(V <sub>CC</sub> -1)	V
T <sub>oper</sub>	Operating Temperature Range LS204C LS204I	0 to +70 -40 to +105	°C
P <sub>tot</sub>	Power Dissipation at T <sub>amb</sub> = 70°C <sup>1)</sup>	500	mW
T <sub>J</sub>	Junction Temperature	150	°C
T <sub>stg</sub>	Storage Temperature Range	-65 to +150	°C

<sup>1.</sup> Power dissipation must be considered to ensure maximum junction temperature (Tj) is not exceeded.

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# **ELECTRICAL CHARACTERISTICS**

 $V_{CC} = \pm 15V$ ,  $T_{amb} = 25$ °C (unless otherwise specified)

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Councile ad	Davamatan	LS204I				LS204C		l lmit
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Symbol	Parameter	Min.	Тур.	Max.	Min.	Тур.	Max.	Unit
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	I <sub>cc</sub>			0.7	1.2		0.8	1.5	mA
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I <sub>ib</sub>	T <sub>amb</sub> = 25°C		50			100		nA
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R <sub>i</sub>	Input Resistance (f = 1kHz)		1			1		ΜΩ
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$V_{io}$	$T_{amb}$ = 25°C $T_{min}$ < $T_{op}$ < $T_{max}$		0.5			0.5		mV
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$DV_io$			5			5		μV/°C
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I <sub>io</sub>			5			12		nA
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	DI <sub>io</sub>			0.08			0.1		nA/°C
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I <sub>os</sub>	Output Short-circuit Current		23			23		mA
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	A <sub>vd</sub>	$T_{min} < T_{op} < T_{max}$ $R_L = 2k\Omega$ $V_{CC} = \pm 15V$	90			86			dB
$\begin{array}{c} e_n \\ e_n \\ R_s = 50\Omega \\ R_s = 10k\Omega \\ R_s = 10k\Omega \\ \end{array} \\ \begin{array}{c} R_s = 100\Omega \\ R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \end{array} \\ \begin{array}{c} R_s = 10k\Omega \\ \end{array} \\ \begin{array}{c}$	GBP	Gain Bandwith Product (f =100kHz)	1.8	3		1.5	2.5		MHz
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	e <sub>n</sub>	$f = 1kHz$ , $R_s = 100\Omega$ $R_s = 50\Omega$ $R_s = 1k\Omega$		10			12		<u>nV</u> √Hz
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	THD			0.03			0.03		%
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	±V <sub>opp</sub>	$R_L = 2k\Omega$ $V_{CC} = \pm 15V$	±13	±3		±13	±3		٧
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	V <sub>opp</sub>			28			28		Vpp
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	SR	Slew Rate ( $R_L = 2k\Omega$ , unity gain)	0.8	1.5			1		V/μs
$ \begin{array}{c c} CMR & V_{ic} = \pm 10V \\ T_{min} < T_{op} < T_{max} \end{array} \qquad \qquad 90 \qquad \qquad 86 \qquad \qquad 86 $	SVR	$T_{min} < T_{op} < T_{max}$	90			86			dB
V <sub>01</sub> /V <sub>02</sub> Channel Separation (f= 1kHz) 100 120 120 dB	CMR	$V_{ic} = \pm 10V$	90			86			dB
	V <sub>01</sub> /V <sub>02</sub>	Channel Separation (f= 1kHz)	100	120			120		dB

Figure 1: Supply Current versus Supply Voltage

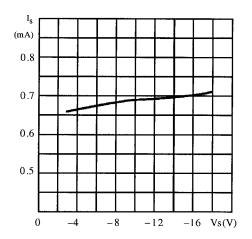


Figure 3: Output Short Circuit Current versus Ambient Temperature

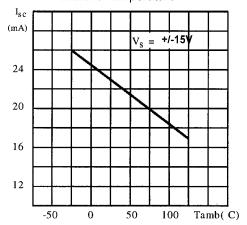


Figure 5 : Output Loop Gain versus Ambient Temperature

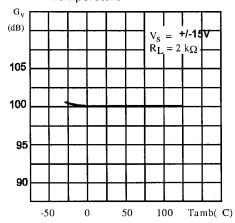
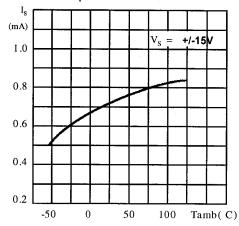


Figure 2: Supply Current versus Ambient Temperature



**Figure 4 :** Open Loop Frequency and Phase Response

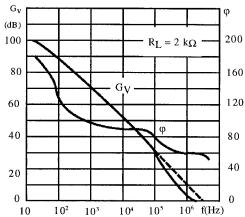
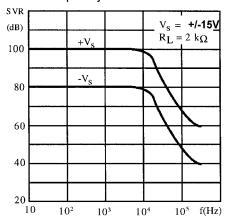


Figure 6 : Supply Voltage Rejection versus Frequency



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Figure 7: Large Signal Frequency Response

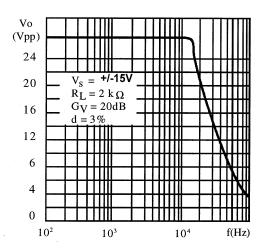
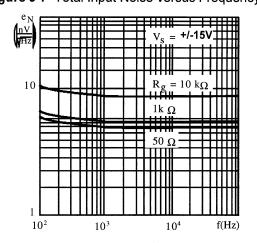


Figure 9: Total Input Noise versus Frequency



**Figure 8 :** Output Voltage Swing versus Load Resistance

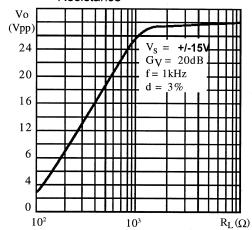
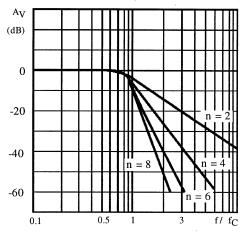
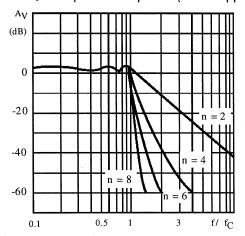


Figure 10: Amplitude Response



**Figure 11:** Amplitude Response ( ±1dB ripple)



### **APPLICATION INFORMATION: Active low-pass filter**

#### **BUTTERWORTH**

The Butterworth is a "maximally flat" amplitude response filter (figure 10) Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in samples-data applications and for general purpose low-pass filtering.

The cut-off frequency Fc, is the frequency at which the amplitude response is down 3dB. The attenuation rate beyond the cutoff frequency is n6 dB per octave of frequency where n is the order (number of poles) of the filter.

Other characteristics:

- ☐ Flattest possible amplitude response
- ☐ Excellent gain accuracy at low frequency end of passband

#### **BESSEL**

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

The maximum phase shift is  $\frac{-n\pi}{2}$  radians where

n is the order (number of poles) of the filter. The cut-off frequency fc, is defined as the frequency at which the phase shift is one half of this value.

For accurate delay, the cut-off frequency should be twice the maximum signal frequency.

The following table can be used to obtain the -3dB frequency of the filter.

	2 Pole	4 Pole	6 Pole	8 Pole
-3dB Frequency	0.77fc	0.67fc	0.57fc	0.50fc

Other characteristics:

- ☐ Selectivity not as great as Chebyschev or Butterworth
- Very little overshoot response to step inputs
- ☐ Fast rise time

#### **CHEBYSCHEV**

Chebyschev filters have greater selectivity than either Bessel ro Butterworth at the expense of ripple in the passband (figure 11).

Chebyschev filters are normally designed with peak-to-peak ripple values from 0.2dB to 2dB.

Increased ripple in the passband allows increased attenuation above the cut-off frequency.

The cut-off frequency is defined as the frequency at which the amplitude response passes through the specificed maximum ripple band and enters the stop band.

Other characteristics:

- Greater selectivity
  - Very non-linear phase response
- ☐ High overshoot response to step inputs

The table below shows the typical overshoot and setting time response of the low pass filters to a step input.

	Number of Poles	Peak Overshoot	Settling	Time (% of fina	al value)
		% Overshoot	±1%	±0.1%	±0.01%
	2	4	1.1Fc sec.	1.7Fc sec.	1.9Fc sec.
Duttomuorth	4	11	1.7/fc	2.8/fc	3.8/fc
Butterworth	6	14	2.4/fc	3.9S/fc	5.0S/fc
	8	14	3.1/fc	5.1/fc	7.1/fc
	2	0.4	0.8/fc	1.4/fc	1.7/fc
Bessel	4	0.8	1.0/fc	1.8/fc	2.4/fc
	6	0.6	1.3/fc	2.1/fc	2.7/fc
	8	0.1	1.6/fc	2.3/fc	3.2/fc
	2	11	1.1/fc	1.6/fc	-
Chabysachay (ripple + 0.25dD)	4	18	3.0/fc	5.4/fc	-
Chebyschev (ripple ±0.25dB)	6	21	5.9/fc	10.4/fc	-
	8	23	8.4/fc	16.4/fc	-
	2	21	1.6/fc	2.7/fc	
Chabyaahay (ripple + 1dP)	4	28	4.8/fc	8.4/fc	-
Chebyschev (ripple ±1dB)	6	32	8.2/fc	16.3/fc	-
	8	34	11.6/fc	24.8/fc	-

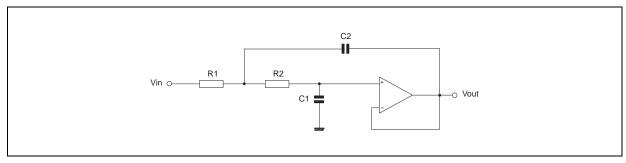
Design of 2nd order active low pass filter (Sallen and Key configuration unity gain op-amp)

Fixed R = R1 = R2, we have (see figure 12)

$$C1 = \frac{1}{R} \frac{\zeta}{\omega c}$$

$$C2 = \frac{1}{R} \frac{1}{\xi \omega c}$$

Figure 12: Filter Configuration



Three parameters are needed to characterize the frequency and phase response of a 2nd order active filter: the gain (Gv), the damping factio ( $\xi$ ) or the Q factor (Q = 2  $\xi$ )<sup>1</sup>), and the cuttoff frequency (fc).

The higher order response are obtained with a series of 2nd order sections. A simple RC section is introduced when an odd filter is required.

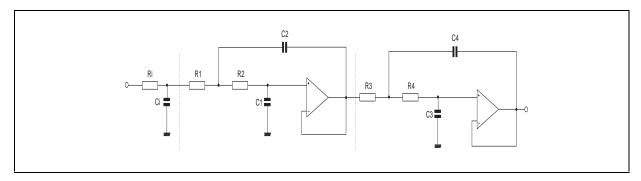
The choice of  $\xi'$  (or Q factor) determines the filter response (see table 1).

Table 1

Filter Response	ξ	Q	Cuttoff Frequency fc
Bessel	$\frac{\sqrt{3}}{2}$	$\frac{\sqrt{1}}{3}$	Frequency at which Phase Shift is -90°C
Butterworth	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{1}}{2}$	Frequency at which Gv = -3dB
Chebyschev	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{1}}{2}$	Frequency at which the amplitude response passes through specified max. ripple band and enters the stop bank.

### **EXAMPLE**

Figure 13: 5th Order Low-pass Filter (Butterworth) with Unity Gain configuration



In the circuit of figure 13, for fc = 3.4kHz and  $R_i$  = R1 = R2 = R3 =  $10k\Omega$ , we obtain:

Ci = 1.354 
$$\frac{1}{R} \frac{1}{2\pi fc}$$
 = 6.33nF  
C1 = 0.421  $\frac{1}{R} \frac{1}{2\pi fc}$  = 1.97nF  
C2 = 1.753  $\frac{1}{R} \frac{1}{2\pi fc}$  = 8.20nF  
C3 = 0.309  $\frac{1}{R} \frac{1}{2\pi fc}$  = 1.45nF  
C4 = 3.325  $\frac{1}{R} \frac{1}{2\pi fc}$  = 15.14nF

The attenuation of the filter is 30dB at 6.8kHz and better than 60dB at 15kHz.

The same method, referring to table 2 and figure 14 is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in table 2. For fc = 5kHz and Ci = C1 = C2 = C3 = 1nF we obtain:

$$Ri = \frac{1}{0.354} \frac{1}{C} \frac{1}{2\pi fc} = 25.5 k\Omega$$

$$R1 = \frac{1}{0.421} \frac{1}{C} \frac{1}{2\pi fc} = 75.6 \text{k}\Omega$$

$$R2 = \frac{1}{1.753} \frac{1}{C} \frac{1}{2\pi fc} = 18.2 \text{k}\Omega$$

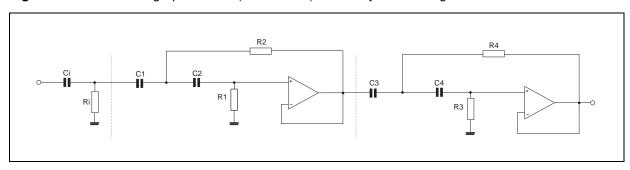
$$R3 = \frac{1}{0.309} \frac{1}{C} \frac{1}{2\pi fc} = 103 \text{k}\Omega$$

$$R4 = \frac{1}{3.325} \frac{1}{C} \frac{1}{2\pi fc} = 9.6k\Omega$$

Table 2: Damping Factor for Low-pass Butterworth Filters

Order	Ci	C1	C2	C3	C4	C5	C6	<b>C</b> 7	C8
2		0.707	1.41						
3	1.392	0.202	3.54						
4		0.92	1.08	0.38	2.61				
5	1.354	0.421	1.75	0.309	3.235				
6		0.966	1.035	0.707	1.414	0.259	3.86		
7	1.336	0.488	1.53	0.623	1.604	0.222	4.49		
8		0.98	1.02	0.83	1.20	0.556	1.80	0.195	5.125

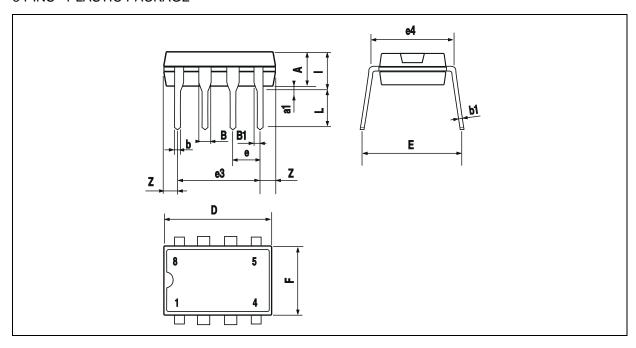
Figure 14: 5th Order High-pass Filter (Butterworth) with Unity Gain configuration



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## PACKAGE MECHANICAL DATA

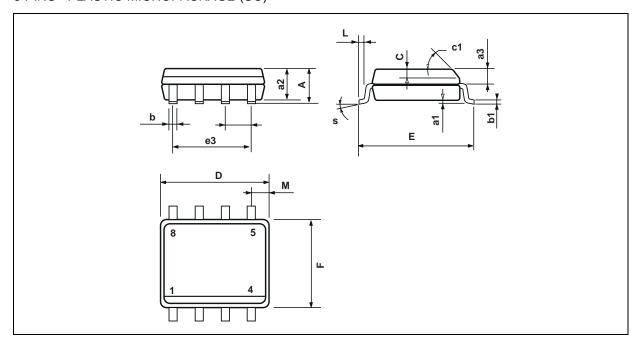
8 PINS - PLASTIC PACKAGE



<b>D</b> :		Millimeters			Inches	
Dimensions	Min.	Тур.	Max.	Min.	Тур.	Max.
Α		3.32			0.131	
a1	0.51			0.020		
В	1.15		1.65	0.045		0.065
b	0.356		0.55	0.014		0.022
b1	0.204		0.304	0.008		0.012
D			10.92			0.430
Е	7.95		9.75	0.313		0.384
е		2.54			0.100	
e3		7.62			0.300	
e4		7.62			0.300	
F			6.6			0260
i			5.08			0.200
L	3.18		3.81	0.125		0.150
Z			1.52			0.060

#### **PACKAGE MECHANICAL DATA**

8 PINS - PLASTIC MICROPACKAGE (SO)



Dimensions		Millimeters			Inches			
אווופוואוטווא	Min.	Тур.	Max.	Min.	Тур.	Max.		
А			1.75			0.069		
a1	0.1		0.25	0.004		0.010		
a2			1.65			0.065		
a3	0.65		0.85	0.026		0.033		
b	0.35		0.48	0.014		0.019		
b1	0.19		0.25	0.007		0.010		
С	0.25		0.5	0.010		0.020		
c1			45°	(typ.)				
D	4.8		5.0	0.189		0.197		
E	5.8		6.2	0.228		0.244		
е		1.27			0.050			
e3		3.81			0.150			
F	3.8		4.0	0.150		0.157		
L	0.4		1.27	0.016		0.050		
M			0.6			0.024		
S			8° (	(max.)	•	•		

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